



## Moderator Temperature Coefficient – MTC

The moderator temperature coefficient – MTC is defined as the change in reactivity per degree change in moderator temperature.

$$\alpha_M = \frac{d\rho}{dT_M}$$

It is expressed in units of pcm/°C or pcm/°F. The value of moderator temperature coefficient usually ranges from 0 pcm/°C to -80 pcm/°C. The **moderator temperature coefficient's** magnitude and sign (+ or -) is primarily a function of the **moderator-to-fuel ratio**. That means it primarily depends on a specific reactor design. It must be noted, according to the design requirements (e.g., [NUREG-0800, Chapter 4](#)), reactor design must assure that:

*“The MTC should be non-positive over the entire fuel cycle when the reactor is at a significant power level.”*

Therefore all [light water reactors](#) (LWR) must be designed **under moderated** because it ensures that the reactor may have a **negative moderator temperature coefficient**. If a reactor is over moderated, it can not reach a positive moderator temperature coefficient. A negative moderator temperature coefficient is desirable because of its **self-regulating effect**.

The total amount of reactivity, which is inserted to a reactor core by a specific change in the

moderator temperature, is usually known as the **moderator reactivity defect** and is defined as:

$$d\rho = \alpha \cdot dT$$

Example: moderator defect

**The moderator temperature coefficient** for a reactor is  $-30 \text{ pcm}/^\circ\text{C}$ .

Calculate the reactivity defect that results from a temperature increase of **20°C**.

Solution:

$$d\rho = \alpha \cdot dT = -30 * 20 = -600 \text{ pcm}$$

The reactivity addition due to the moderator temperature increase is negative about  $-1 \text{ \$}$  (for reactor core with  $\beta_{\text{eff}} = 0.006$ ).

### Theory of Moderator Temperature Coefficient

It is very difficult to describe the physics of the moderator temperature coefficient because changes in **moderator temperature** lead to the change of almost **all the parameters** in a reactor core. For better understanding, we describe major physical mechanisms that occur in the **moderator temperature coefficient** in terms of the [six-factor formula](#).

$$\uparrow T_M \Rightarrow \downarrow k_{\text{eff}} = \eta \cdot \epsilon \cdot \downarrow p \cdot \uparrow f \cdot \downarrow P_f \cdot \downarrow P_t \text{ (BOC)}$$

$$\uparrow T_M \Rightarrow \downarrow k_{\text{eff}} = \eta \cdot \epsilon \cdot \downarrow p \cdot f \cdot \downarrow P_f \cdot \downarrow P_t \text{ (EOC)}$$

**Major impacts** on the multiplication of the system arise from the change of [the resonance escape probability](#) and the change of total neutron leakage (see [thermal non-leakage probability](#) and [fast non-leakage probability](#)). But as can be seen at the beginning of the cycle (BOC), when the PWR core contains a large amount of boron dissolved in the primary coolant ([chemical shim](#)), an increase in temperature causes an increase in the [thermal utilization factor](#).

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**Change of the resonance escape probability.** It is known, **the resonance escape**

**probability** is also dependent on the **moderator-to-fuel ratio**. All **PWRs** are designed as under moderated reactors. As the **moderator temperature** increases, the ratio of the moderating atoms (molecules of water) decreases due to the **thermal expansion of water**. Its density simply decreases. This, in turn, causes **hardening of neutron spectrum** in the reactor core resulting in **higher resonance absorption** (lower  $p$ ). The decreasing density of the moderator causes that **neutrons** stay at a higher energy for a longer period, which increases the probability of non-fission capture of these neutrons. It must be added moderator density changes are not linear. At high temperatures, an increase in the moderator temperature causes a larger reduction in density than an identical increase at low moderator temperatures. This process (the **hardening of the neutron spectrum**) is one of two key processes that determine the **moderator temperature coefficient (MTC)**. The second process is connected with the **leakage probability** of the neutrons.

- **Change of the neutron leakage.** Since both ( $P_f$  and  $P_t$ ) are affected by a change in **moderator temperature** in a heterogeneous water-moderated reactor and the directions of the feedbacks are the same, the resulting **total non-leakage probability** is also sensitive to the change in the moderator temperature. As a result, an **increase in the moderator temperature** causes that the probability of **leakage to increase**. In the case of the **fast neutron leakage**, the moderator temperature influences **macroscopic cross-sections** for **elastic scattering reaction** ( $\Sigma_s = \sigma_s \cdot N_{H_2O}$ ) due to the **thermal expansion of water**, which increases the **moderation length**. This, in turn, causes an increase in the leakage of fast neutrons.

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